# Electrical System Design and Installation of New Building, Aisyiyah University, Yogyakarta

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**Abstract** –Aisyiyah University New Yogyakarta Building is one of the commercial buildings that moves the field of education in Yogyakarta. The New Building of Aisyiyah University Yogyakarta consists of 10 floors, including the basement floor, main floor and roof floor. Electric loads installed at the New Building of Aisyiyah University Yogyakarta include lighting loads (lights) and power loads (sockets) and the power loads of electric motors (air conditioners, elevators and others), which of course requires a large enough electricity supply. Electricity installed in the New Building of Aisyiyah University in Yogyakarta is 1010.9 kVA. The power supplied is 800 kVA from State Electricity Company and the total power capacity of the transformer is 1000 kVA and a generator set with a capacity of 1000 kVA. Where the backup power supply system is fully supplied by the generator set.

**Keywords**: Electrical Installation, Artificial Lighting, Short-circuit Current, Power Distribution, Drop Voltage

# I. Introduction

As one of the facilities and infrastructure to support the learning process, a university needs to pay attention to the quality of service facilities and infrastructure in order to provide a sense of comfort and peace for students and their community. This comfort and peace will not be obtained without the presence of good supporting facilities and infrastructure from universities. In the construction of a building in general and universities in particular, it is inseparable from the need for electrical energy. In a building, electrical energy is needed, ranging from lighting systems to lightning protection systems. Therefore, it is necessary to design a system and electrical installation at universities.

In designing an electrical installation a tertiary institution must comply with the provisions of the General Electrical Installation Requirements and the Indonesian National Standard so that electrical energy can be used safely, reliably and effectively [1]. This design is made with the intent and purpose to understand the general rules of electrical installation and can learn and know how to design, install, check, test, maintain and supervise an electrical installation. A high-performance electrical installation design needs to be designed in detail so as not to over-design.

# II. Methods

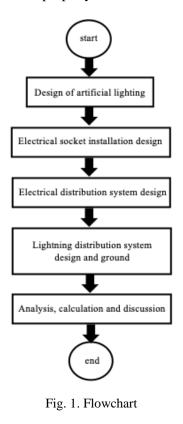
Flowchart for the research is presented in Fig. 1. 1. Designing system design

Starting from the design of artificial lighting systems, installation of contact boxes, electrical distribution system design, lightning protection systems and grounding systems using the AutoCAD application.

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2. Analysis, calculation, and discussion of electrical installation system design

All systems that have been made will be analyzed and calculated and considered whether all systems are in accordance with installation standards and the system will work properly.



#### **III.** Results

#### III.1. Determination of the Number of Lamp Armature Points

The following is a calculation for one of the rooms on the 4th floor:

- 1. Main room
  - Type of lamp to be installed = 14 Watt LED Lamps
  - Luminous lamp flux ( $\Phi$ ) = 1400 lumens
  - Lux room according to SNI (E) = 350 Lux
  - Run area (A) =  $290 \text{ m}^2$
  - Light loss factor (LLF) = 0.8
  - Utility factor (CU) = 100% (estimated)

$$N = \frac{E x A}{\phi x LLF x CU x n}$$
$$N = \frac{350 x 290}{1400 x 0.8 x 100\% x 1} = 90,625$$
(1)

So, the minimum number of light points needed is as many as 91 points.

As for the calculation of another room on the same floor using a light loss factor (LLF) of 0.8 and a utility factor (CU) of 100% are presented in Table I [2].

CALCULATION OF NUMBER OF LAMP POINTS 4 <sup>TH</sup> FLOOR					
No.	Room Names	Large	Lux	Amount ideal	
1	Main room	290	350	91	
2	Stair Area 2	24	100	3	
3	Stair Area 1	21	100	3	
4	Lobby Side Services	23.5	100	3	
5	Corridor	160	100	20	
6	Men's Toilet	11	250	4	
7	Women's Toilet	13	250	4	
8	Janitor	3.5	100	1	
9	Special Toilet	4	250	1	
10	Male Ablution Room	1.3	250	1	
11	Women's Ablution Room	1.3	250	1	
12	Nursing Room	2	250	1	
13	Panel Room	3	250	1	
14	Room 01	102	250	23	
15	Room 02	98	250	22	
16	Room 03	98	250	22	
17	Room 04	101	250	23	
18	Room 05	59	250	13	
19	Room 06	59	250	13	

#### TABLE I CALCULATION OF NUMBER OF LAMP POINTS 4<sup>th</sup> Floor

## III.2. Panel Load Schedule

Lighting panel and 4th floor contact box. All MCB group ratings on the 4th floor LP & PP panel are 16A.

1. MCB group 1 (PL-4/01)

- Installed Load:

- LED Lamps 14W x 93 pieces = 1302 Watt
- LED Lamps 14W + Battery x 7 pieces = 98 Watts
- Total installed load power (P) = 1400 Watt
- Voltage (V) / Phase / Frequency (F) = 220V
   / 1 / 50Hz (State Electricity Company)
- Assumption  $\cos \Phi = 0.85$
- Installed load current (I):

$$I = \frac{P}{V_{LN} * COS \phi} = \frac{1400}{220 * 0.85} = 7.49 \, \text{A}$$
(2)

The calculation for the next MCB group with the assumption strength of each outlet is 100W and uses

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equation 2, as presented in Table II.

CALCULATION OF THE 4TH FLOOR PANEL LOAD SCHEDULE					
No.	Group	Load Type	Load	Current	
INO.	Panel	Installed	(W)	Load	
1	PL-4/01	Led lamps 14W	1302	7.49	
1	FL-4/01	+ Battery	98	7.49	
2	PL-4/02	Led lamps 10W	360	2.25	
2	I L-4/02	+ Battery	60	2.23	
		Led lamps 10W	120		
3	PL-4/03	+ Battery	20	0.89	
5	1 L-4/03	Led T8 9W	18	0.07	
		+ Battery	9		
4	PL-4/04	Led lamps 14W	406	2.25	
-	I L-4/04	+ Battery	14	2.23	
5	PL-4/05	Led lamps 14W	406	2.25	
5	1 L-4/05	+ Battery	14	2.23	
6	PL-4/06	Led lamps 14W	406	2.25	
0	1 L-4/00	+ Battery	14	2.23	
7	PL-4/07	Led lamps 14W	406	2.25	
,	1 L-4/07	+ Battery	14	2.25	
8	PL-4/08	Led lamps 14W	224	1.27	
0	1 L-4/00	+ Battery	14	1.27	
9	PL-4/09	Led lamps 14W	224	1.27	
,	I L-4/07	+ Battery	14	1.27	
10	ES-4/01	Wall ES 40 cm	400	2.67	
10	L5 4/01	Wall ES 150 cm	100	2.07	
		Wall ES 40 cm	400		
11	ES-4/02	Floor ES	125	4.14	
		Projector ES	250		
		Wall ES 40 cm	400		
12	ES-4/03	Floor ES	125	4.14	
		Projector ES	250		
		Wall ES 40 cm	400		
13	ES-4/04	Floor ES	125	4.14	
		Projector ES	250		
		Wall ES 40 cm	400		
14	ES-4/05	Floor ES	125	4.14	
		Projector ES	250		
1.5		Wall ES 40 cm	200	4.1.4	
15	ES-4/06	Wall ES 150 cm	200	4.14	
1.4		Floor ES	125	2.1.1	
16	ES-4/07	Wall ES 40 cm	400	2.14	
17	ES-4/08	Wall ES 40 cm	400	2.14	
18	ES-4/09	Floor ES	125	3.34	
10	EC 4/10	Projector ES	500		
19	ES-4/10	Wall ES 40 cm	600	3.21	
20	EC 4/11	Wall ES 40 cm	200	4 1 4	
20	ES-4/11	Wall ES 150 cm	200	4.14	
		Floor ES	125		

TABLE II LATION OF THE 4TH FLOOR PANEL LOAD S

# 2. Main room

Loads from all groups are divided into phases R, S and T, so that the load current installed in the three phases is balanced or close. The distribution of the full load can be seen in the appendix chapter, each value of installed load current per phase of the sum of all groups is as follows.

- Phase R (IR) = 19.0 A
- Phase S (IS) = 18.8 A
- Phase T (IT) = 19.3 A

3. Main Circuit Breaker (CB)

Main CB is the main circuit breaker for this panel.

- Built-in load current (I) = 19.3 A in phase R (taken only from the phase that has the highest value)
- Minimum current carrying capacity (CRC) cable installation (I CRC ):
- I KHA = I \* 125% = 19.3 \* 125% = 24.2 A
- The type of CB selected is a fixed-phase 3phase MCCB (molded case circuit breaker), because it has a high resistance to heat.
- The MCCB rating must be higher than the group MCB rating (16A) and the installation cable CRC (I KHA = 24.125 A).
- For future load growth reserves, the chosen rating is 30A, according to the brochure available on the market.

4. Feeder cable

Feeder cable, pulled from SDP Gedung to PL & PP 4th Floor panel.

- The *grounding* cable used is bare copper cable, which is the BCC cable.
  Minimum cable cross
  - sectional area (A GROUND):
- $A GROUND = A FEEDER * 50\% = 6 \text{mm}^2 \text{ x}$ 50% = 3 mm<sup>2</sup>
- In accordance with the available brochure, the selected *grounding* cable is BCC 6mm<sup>2</sup>

#### III.3. LVMDP Load Schedule

1. Distribution of Loads to Phase R, S, and T

After multiplying by the simultaneity factor, the estimated load which was previously 840.0 kVA (installed electrical load) becomes 663.8 kVA (normal maximum load). Then, the electric current can be calculated, as follows.

- Phase R (IR) = 1011.2 A
- Phase S (IS) = 1018.6 A
- Phase T (IT) = 1011.9 A

2. Main Circuit Breaker (CB)

Main CB is the main circuit breaker for this panel.

- Built-in load current (I) = 1018.6 A in phase S (taken only from the phase that has the highest value).
- The type of CB selected is a 3 phase MCCB (*miniature circuit breaker*) fix type, because it has a high resistance to heat.
- For future load growth reserves, the chosen rating is 1250A, according to the brochure

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available on the market.

3. Feeder cable

Feeder cable, pulled from transformer to LVMDP

- Minimum current carrying capacity (CRC) cable installation (I CRC ):
- I KHA = I \* 125% = 1018.6 \* 125% = 1273.25 A
- The feeder cable used is copper cable with double PVC insulation, i.e. NYY cable.
- The cable used consists of four cores; that is, for phase R, phase S, phase T and neutral.
- The cable CRC must not be less than 1250A (main MCCB rating) and should consider Voltage drop on the cable.
- In accordance with the available brochure, the chosen cable is NYY 4 x (4 x 1 x 300mm<sup>2</sup>) with a CRC of 2208A.
- 4. Grounding cable

Grounding cable, pulled from the Grounding Well to LVMDP.

- The *grounding* cable used is bare copper cable, which is the BCC cable.
- Minimum cable crosssectional area (A GROUND):
- $A GROUND = A FEEDER * 50\% = (4 \times 300)$ mm<sup>2</sup> x 50% = 2 x 300mm<sup>2</sup>
- In accordance with the available brochure, the selected *grounding* cable is 2 x BCC 300  $\text{mm}^2$

#### III.4. Power Factor Improvement

After getting the total amount of apparent power and active power, then the reactive power calculation can be done in order to determine the capacity of the capacitor bank that is needed as an effort to improve the power in the building [3]. The formula to be used in calculating reactive power is presented in equation 3.

$$Q = \sqrt{S^2 - P^2} \tag{3}$$

Information: Q = reactive power (VAR) S = Pseudo power (VA) P = Active power (W)

# 1. Determine the total reactive power (VAR)

Determine the amount of reactive power obtained from apparent power and active power that has been

multiplied by the togetherness factor (estimation). The apparent power = 663.9 kVA and active power = 546.7 kW so that the following calculation is presented in equation 4.

$$Q = \sqrt{S^2 - P^2}$$
  

$$Q = \sqrt{663,9^2 - 546,7^2}$$
  

$$Q = 376,54 \text{ Kvar}$$
(4)

2. Determine the value of  $\cos \Phi$  (phi) before power repair

The value of Cos  $\Phi$  (phi) before the power factor improvement is obtained by calculating as presented in equation 5.

$$Cos \Phi = \frac{546,7}{663,9}$$
  
Cos  $\Phi = 0.82$  (5)

From equation 5, the initial  $\cos \Phi$  (phi) found on the Aisyiyah University Yogyakarta campus is 0.82 while  $\cos \Phi$  required for the building is 0.92. The calculation of the capacitor capacity of the bank to be installed is presented in equation 6.

$$S1 = \frac{P}{0.92}$$
  

$$S1 = \frac{546.7}{0.92}$$
  

$$S1 = 594.2 \text{ kVA}$$
(6)

So the reactive power calculation if  $\cos \Phi$  is 0.92, as presented in equation 7.

$$Q1 = \sqrt{S1^2 - P^2}$$

$$Q1 = \sqrt{594,2^2 - 546,7^2}$$

$$Q1 = 232,89 \text{ kVAR}$$
(7)

From the calculation of Cost  $\Phi$  of 0.92, it can be determined the amount of bank capacitors to be used, as presented in equation 8.

$$C = Q - Q1$$
  

$$C = 376,54 - 232,89$$
  

$$C = 143,7 \text{ kVAR}$$
(8)

Then the amount of bank capacitors to be used on the campus of Yogyakarta Aisyiyah University is 143.7 kVAR with a combination of 12x25 kVAR. 12x25 kVAR combination is chosen, because the

rest is used as a backup if one day there is damage or overreactive power.

#### III.5. Genset and Transformer Capacity

The main principle in determining the capacity of the generator and transformer is that the normal normal load must not exceed 75% of the capacity of the transformer and generator. The calculation that will be used to determine the capacity of the generator set and transformer is as follows:

1. The maximum normal load of buildings

The maximum normal load of buildings after improvement of the power factor is 594.2 kVA

#### 2. Generator Capacity

Generator capacity is presented in equation 9.

$$\frac{594,2}{75\%} = 792,27 \ kVA \tag{9}$$

In accordance with the brochure available and circulating in the market, the capacity of the generator used is 1000 kVA

#### 3. Transformer Capacity

Transformer capacity is presented in equation 10.

$$\frac{594,2}{75\%} = 792,27 \, kVA \tag{10}$$

In accordance with the brochure available and circulating in the market, the capacity of the transformer used is as much as 1000 kVA.

#### 4. State Electricity Company Power

To determine the amount of subscription power that will be connected from State Electricity Company must refer to the estimated maximum normal load and from the State Electricity Company subscription power brochure. From the calculation results, the maximum normal load of Yogyakarta Aisyiyah University is 594.2 kVA, so that according to the power available at PLN's bureau, the power to be connected is 800 kVA

#### III.6. Drop Voltage

Following is an example of calculation of voltage drop from a Transformer to LVMDP Panel:

- Cable Type: NYY 4x (4x1x300 mm<sup>2</sup>)
- $R = 0.075 \ \Omega / kM$
- L = 0.000305 H / kM

- I = 1488.7 A
- X L = 0.09577  $\Omega / kM$
- $\cos \Phi = 0.78$  (Assumption)
- $\sin\Phi = 0.62$
- Drop Voltage is presented in equation 11.

$$\Delta V = \frac{\sqrt{3} x I x l x (R \cos \Phi + X \sin \Phi)}{\Delta V = 1.519670 V}$$
$$\Delta V = \frac{\Delta V}{V} x 100\%$$
$$\Delta V = \frac{1.51555}{380} x 100\%$$
$$\% \Delta V = 0.003999131\%$$
(11)

For each floor height is assumed to be 4 so that the length of the cable from one floor to another is added to 5 meters. The calculations for impendance and voltage drop for other panels are presented in Table III.

	TABLE III						
	CALCULATION OF DROP VOLTAGE						
No	Panel Name	$\Delta V(V)$	ΔV (%)				
	Outgoing LVMDP						
1	SDP Building	2.511	0.006607695				
2	SDP Pump	0.148868	0.000391759				
3	PK STP	0.168856	0.000444357				
4	PP Power House	0.098499	0.000259208				
	SDP Building						
1	SDP Lift	0.665882	0.001752320				
2	PC Pressurise Fan	0.073431	0.000193239				
3	PP Electronic	0.058418	0.000153730				
4	LP & PP SB Floor	0.328458	0.000864364				
5	LP & PP 1st Floor	0.170239	0.000447998				
6	PP AC 1st Floor	0.319234	0.000840091				
7	LP & PP 2nd Floor	0.232693	0.000612350				
8	PP AC 2nd Floor	0.400941	0.001055107				
9	LP & PP 3rd Floor	0.265828	0.000699547				
10	PP AC 3rd Floor	0.347713	0.000915035				
11	PP Server	0.410922	0.001081375				
12	LP & PP 4th Floor	0.412749	0.001086181				
13	PP AC 4th Floor	0.565592	0.001488401				
14	LP & PP 5th Floor	0.503282	0.001324427				
15	PP AC 5th Floor	0.648195	0.001705776				
16	LP & PP 6th Floor	0.565459	0.001488049				
17	PP AC 6th Floor	0.768230	0.002021658				
18	LP & PP 7th Floor	0.925391	0.002435239				
19	PP AC 7th Floor	0.662977	0.001744675				
20	LP & PP 8th Floor	1.036764	0.002728326				
21	PP AC 8th Floor	1.200454	0.003159090				
22	SDP Roof	0.828414	0.002180036				

## III.7. Short Circuit Current

Calculation of short-circuit current in the transformer [4]. The following are the specifications listed on the transformer:

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- Transformer apparent power (SrT) = 1000 kVA
- Transformer voltage (UrT) = 20 kV / 0.4 kV
- Number of phases = 3
- Short circuit voltage (Ukr) = 5%.
- Total transformer loss (PkrT) = 13 kW

To get a large short circuit current in a transformer, first look at the total impedance value in the transformer, which is presented in equation 12.

$$Z_T = \frac{U_{kr}}{100\%} x \frac{U_{r\ TLV}^2}{S_{rT}} = \frac{5\%}{100\%} x \frac{0.4^2}{1000}$$
$$Z_{\text{THV}} = 8 \text{ m}\Omega$$

$$R_T = P_{KrT} x \frac{U_{r_T}^2}{S_{rT}^2} = 13 x \frac{0.4^2}{1000^2}$$
$$R_T = 2.08 \text{ m}\Omega$$

$$U_{Rr} = 100\% x \frac{P_{krT}}{S_{rT}} = 100\% x \frac{13}{1000}$$
$$U_{Rr} = 1,3\%$$

$$U_{Xr} = \sqrt{U_{Kr}^{2} - U_{Rr}^{2}} = \sqrt{5^{2} - 1.3^{2}}$$
$$U_{Xr} = 4,828 \%$$

$$X_T = \sqrt{Z_T^2 - R_T^2} = \sqrt{8^2 - 2,08^2}$$
$$X_T = 7,725 \text{ m}\Omega$$

$$K_T = 0.95 \frac{C_{max}}{1 + 0.6X_T} = 0.95 \frac{1.1}{1 + 0.6 * 7.725}$$
$$K_T = 1.015580404$$
(12)

So the results of the calculation of the 3 phase short circuit sismetric short circuit on the transformer are presented in equation 13.

$$Z_T = \sqrt{R_T^2 + X_T^2} = \sqrt{2,08^2 + 7,725^2}$$
$$Z_T = 8 \text{ m}\Omega$$

$$Z_{TK} = Z_T * K_T = 8 * 1.015580404$$
  
$$Z_{TK} = 8,125 \text{ m}\Omega$$
(13)

So that the 3-phase symmetry short circuit current can be calculated in the transformer, as presented in equation 14.

$$I^{n}K = \frac{C * U_{n}}{\sqrt{3} * Z_{TK}} = \frac{1.1 * 400}{\sqrt{3} * 8,125}$$
$$I^{n}K = 31,26711058 \text{ kA}$$
(14)

Based on equation 14, the initial short-circuit current is 31.27 kA

#### III.8. Building Protection Level

Based on the General Rules of Lightning Arrangement Installation in Indonesia, the magnitude of the need for installing lightning arrest system against lightning strikes in a building is determined by adding up the indices that represent the situation in the location of the structure is located. Then for the building indexes are obtained as follows:

1. Index A, Usage and Content Index A

Use and Content of Yogyakarta Aisyiyah University Building Planning is an educational building with an Index Value = 3.

#### 2. Index B, Building Construction

This building includes buildings with reinforced concrete construction or iron frames with non-metal roofs. Index Value = 2.

#### 3. Index C, Building Height

This building has a height of up to 35 meters. Index Value = 5

#### 4. Index D, Building Situation

This building is on a flat ground at all height with an index value = 0.

#### 5. Index E, lightning effect

Based on the number of thunder days per year to reach 182.5 days per year, then the Index Value E =8. Total number the index value above is in accordance with the equation R = A + B + C + D + E obtained the value of R = 18 Then the estimated danger of lightning strikes is very large and securing lightning strikes against buildings is very necessary [5].

## III.9. Election of Lightning Rods

The high lightning rod installed in a building is very influential on the radius of protection, the higher the lightning rod installation, the wider the

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protected area. Based on the Indonesian National Standard number 03-7015-2004 concerning lightning protection systems in buildings, in the New Building, Yogyakarta Aisyiyah University, Flash Vectron lightning rods based on ESE (Early Streamer Emission) will be installed [6].

# IV. Conclusion

Based on the results of the design that has been done in this study, the results obtained are:

- 1. The total active power in planning the construction of the new building of Aisyiyah University in Yogyakarta is 680.7 kW and the total apparent power is 840.0 kVA.
- 2. In an effort to increase cos phi from 0.82 to 0.92, a capacitor bank with a capacity of 143.7 kVAR is required and a capacitor bank with a capacity of 300 kVAR is installed.
- 3. The total active power after being subjected to togetherness in the planning of the new building of Aisyiyah University in Yogyakarta is 546.7 kW and the total apparent power after the power factor improvement is 594.2 kVA.
- 4. The maximum total normal load after the capacitor bank is installed is 594.2 kVA. Then the PLN power connection can be chosen, namely medium voltage capacity of 800 kVA, 3 phase, 50Hz.
- 5. The selected transformer capacity and generator capacity is 1000 kVA.
- 6. Lightning strikes against the new building of Aisyiyah University Yogyakarta are very large and securing lightning strikes against buildings is needed, therefore lightning rods chosen to protect buildings from lightning strikes are cage based Flash Vectron based on Early Streamer Emission (ESE).

#### Acknowledgements

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