# A Comparative Analysis of Recent MPPT Algorithms (P&O\INC\FLC) for PV Systems

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Abstract—Although solar (PV) power generators have been widely deployed, one important barrier to their effective energy capture is weather variability. It is a very challenging effort for these systems to operate at MPPT. Conventional MPPT methods still had an excessively long convergence period to the MPP. Because of their superior data processing, intelligent approaches are nevertheless given a reasonable length of time to reach the maximum point, beginning with the objective of keeping the PV generator in the MPP with outstanding performance. To accomplish MPPT, a comparison between intelligent (fuzzy control (FLC)) and conventional algorithms (perturb-andobserve (P&O) and the incremental conductance (INC)) is investigated. To do this, a mathematical model of PV cells based on two diodes with shunt and series resistors is created with MATLAB/Simulink. The model characteristics curves with the parameters listed in the MSR SOLAR datasheet are compared. Finally, we compared the results of the FLC with those of the P&O and the INC. The results obtained demonstrated the superiority of the FLC-MPPT controller.

Keywords—Solar Energy; MPPT Methods; Fuzzy Control; Perturb-and-Observe Control; Incremental Conductance Control.

## I. INTRODUCTION

One of the necessities for humankind is electricity, and power system operators have long struggled to supply it with an increasing need via both traditional and unconventional methods. Around the world, utilities are concentrating on renewable energy sources (RESs) like solar (PV), hydro, biomass, and wind energy systems to meet the constantly rising need for power [1]-[8]. In 2021, RESs accounted for 33% of the world's electrical capacity, with PV, wind, and hydropower leading the way. In 2020, it created around 11.5 million employment and avoided more than 2 billion metric tons of CO<sub>2</sub> emissions in 2019. By 2024, RESs capacity addition is expected to have increased by 50%, with PV and wind systems playing a major role in this expansion [9]-[14].

By 2030, it is anticipated that the total investment in the RESs industries will amount to \$2.6 trillion. Current governments are pledging to meet ambitious RESs targets, like the EU's 32% RESs goal for 2030, highlighting the

sector's importance in an RESs future. The surge in the adoption of electric cars is closely linked to the growth of RESs [15]-[18]. A more sustainable way to lessen our reliance on fossil fuels is through RESs. It is also a clean source of energy and requires little upkeep [19]-[21]. Through declining costs, technological advancements that have reduced costs and increased efficiency, and some new government incentives, PV systems are becoming cheaper [22]-[25].

A unidirectional DC-DC boost converter (BC) is utilized to maximize power extraction from the PV since it generates DC power, and an inverter effectively transforms power into AC to satisfy load demands [26]-[29]. The two primary types of PV systems are grid-tied type (GTT) and isolated type (IT). The cost of the IT is considerable because storage tools (STs) are required to sustain the variance in DC power. Installation and maintenance expenses are extremely minimal for GTT categories since they do not need an ST [30]-[32].

The MPPT control is a significant issue in the field of PV systems, we have a problem with the efficiency of energy conversion, and to solve this problem, it's necessary to use the MPPT controller to extract the maximal power (MP) in the PV modules in different climatic conditions [33]-[36]. This leads the scientific research to the development of new electronic components to implement modern controls capable of processing data in a short time to achieve an excellent temporal response in the MPPT control and to apply a sophistic controller on the PV energy conversion system, among the researches carried out in the field of PV system control we have: Ref. [37] realized the incremental conductance control (INC) with a variable increment stepsize (ISS) to improve the performance of the INC with a fixed ISS in terms of response time and accuracy. Refs. [38], [39] proposed the comparative study between the fuzzy logic (FLC) and ANFIS you are using the current and power as input of the FLC and the ANFIS controller to reduce the calculation.



Ref. [40] proposed the modified P&O for extracting MP from the PV. This algorithm is used to eliminate the MPPT deviation to around the MPP. Ref. [41] proposed the FLC-MPPT to solve the problem of the oscillation around the MPP in the P&O. Ref. [42] realized the INC-MPPT by an FLC to reach MP. Ref. [43] uses the neuro FLC to give the standard voltage of the MPP, to ensure the system's overall stability, use the integral backstepping controller. Ref. [44] proposes a modified P&O to extract the MP available, this method is based on power disturbance instead of voltage or current (V\I) disturbance, for the synchronization of powers to inject a sliding mode controller to the networks has been used. Ref. [45] uses an MPPT command based on the knowledge of the load current to extract the MP, unlike the other methods, which are based on the V\I knowledge. Ref. [46] proposes a P&O control with a variable step size to improve the convergence time towards the MPP of the classic P&O control. Ref. [47] proposes a comparative study between the performances of the P&O control and the FLC under partial shading conditions. Ref. [48] realized adaptive FLC based on comparing an FLC's output with a triangular signal to generate the duty cycle that maintains the GPV system in the MPP.

Ref. [49] proposed a comparative study between three MPPT methods: Traditional P&O, drift-free P&O, and amended technique for quickly shifting environmental circumstances. Ref. [50] proposes improving the INC-MPPT to achieve a good follow-up of the MPP. Ref. [51] implemented a PI controller with variable gain. The variation of the PI parameters is carried out with the help of an FLC supervisor; the validation of the performance is achieved with the experimental implementation and a comparison with a classical PI and P&O in MPPT control. Ref. [52] proposed a contrast study of the PV system controlled by the Takagi-Sugeno, FLC Mamdani, and P&O sorts. Refs. [53], [54] proposed an MPPT procedure with optimized PID to increase the performance of the P&O. Ref. [55] proposed a new variable step size INC-MPPT.

To accomplish our goal, which is to extract the MP that is available in a PV system at any given moment, we have suggested in this work a comparison analysis of the control: P&O, INC, and FLC. The remainder of this research is structured as follows: The modeling and simulation of the system components, PV, and boost converter (BC) are covered in Section 2. The MPPT techniques, P&O, INC, and FLC, are presented in Section 3. The properties of the MPPT control are compared and analyzed in part 4, with the main conclusion presented in the last part.

#### II. PV SYSTEM

Fig. 1 displays a diagram of a PV power generation from a PV source which consists of the following elements: PV panel, BC, load charge, and MPPT controller to ensure the operation of the PV at the MPP.

# A. Mathematical Model of PV

Several mathematical models of the PV panel are presented in the literature to simulate all the phenomena existing in an actual panel [56]-[60]. Fig. 2 displays a similar drawing of a PV cell which is made up of an I source

modeling the luminous flux, 2 resistors modeling the losses, a shunt resistor  $(R_p)$ , a series resistor  $(R_s)$ , and 2 diodes for the polarization of the solar cell (SC) and the phenomenon of recombination of the minority carriers. This additional diode is equivalent to the chemical effects of electron recombination. The following equation gives the produced I by the model [61]-[64].

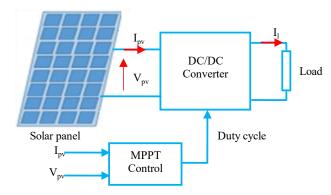


Fig. 1. Principle schema of PV system

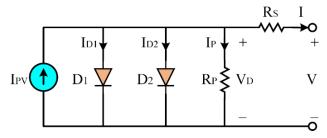


Fig. 2. Diagram of the SC

$$I = I_{PV} - I_{d1} - I_{d2} - \frac{V + IR_s}{R_v}$$
 (1)

The photo-current  $(I_{PV})$  is defined as:

$$I_{PV} = \frac{E}{E_{ref}} [I_{cc} + K_i (T_C - T_{ref})]$$
 (2)

where E is the solar radiation (SR) (W/m<sup>2</sup>),  $E_{ref}$  is the SR of reference 1000 W/m<sup>2</sup>,  $T_c$  is the ambient temperature of SC, and  $T_{ref}$  is the reference temperature ( $T_{ref} = 25$ °C).

The diode current  $(I_d)$  which the Shocly equation can be expressed as:

$$I_d = I_s \left( e^{\frac{q \, Vd}{Ak \, Tc}} - 1 \right) \tag{3}$$

where A is the ideality factor of the diode, k is the Boltzmann constant, q is the electron charge, and  $T_C$  is the SC temperature.

The diode current loss  $(I_s)$  is expressed as:

$$I_{s} = I_{rs} \left(\frac{T}{T_{rof}}\right)^{3} e^{\left[\frac{-qE_{g}}{KA}\left(\frac{1}{K} - \frac{1}{T_{ref}}\right)\right]}$$
(4)

The inverted saturation current  $(I_{rs})$  of the SC is expressed as:

$$I_{rs} = \frac{I_{cc}}{e^{\left(\frac{q \, Voc}{N_{s \, KA \, Tc}}\right)} - 1} \tag{5}$$

where  $E_g$  is the energy for the passage of a free electron between the valence and conduction bands of the semiconductor, ( $N_s$  and  $N_p$ ) are the number of SCs in series and parallel, respectively. So, we will have the current equation of the SC as follows:

$$\begin{split} I &= N_{p}I_{PH} - N_{p}I_{d1}\left(\frac{q(V-Irs)}{e^{A1kTc}} - 1\right) - NpI_{d2}\left(\frac{q(V-Irs)}{e^{A2kTc}} - 1\right) \\ &- \frac{Np}{Ns}\frac{V+Irs}{Rp} \end{split} \tag{6}$$

Fig. 3 displays the features of curves V-I and V-P.

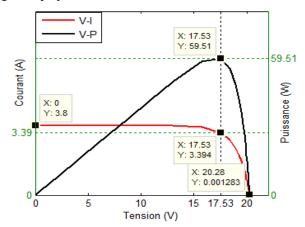


Fig. 3. V-I and V-P panel characteristics curve

To validate our proposed panel model, a comparison was made between the data of the V-I and V-P characteristics curve shown in Fig. 3 with the data of the MSX60 panel model datasheet, as shown in Table I. In addition, the electrical characteristic of the MSX60 module is seen in Table II.

TABLE I. CHARACTERISTICS OF MSX60 MODULE AND PROPOSED PANEL MODULE

	Isc (A)	$V_{oc}\left(V\right)$	$P_{max}(W)$	$V_{opt} \ (V)$	I <sub>opt</sub> (A)
MSX60 module	3.8	21.1	60	17	3.46
Proposed module	3.8	20.28	59.51	17.53	3.39

TABLE II. ELECTRICAL CHARACTERISTIC OF MSX60 MODULE

MP (Pmax)	60W
V (Vmp)	17.1V
I (lmp)	3.5A
$I_{sc}$	3.8A
V	21 1V

#### B. BC Structure and Model

To extract the MP available at a given time, the PV system's BC acts as an adaption element amid the load and the SC. Furthermore, Fig. 4 shows the BC's model brick.

The BC's mathematical model is provided by the next formulas [65]-[68]:

$$\frac{di_L}{dt} = \frac{E}{L} - \frac{V_{dc} (1 - u)}{L} \tag{7}$$

$$\frac{dV_{dc}}{dt} = \frac{i_L (1 - u)}{C} - \frac{V_{dc}}{RC} \tag{8}$$

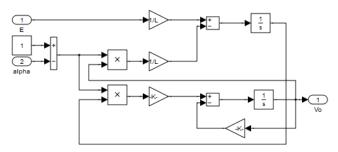


Fig. 4. Simulation block of a BC

#### III. INVESTIGATED MPPT CONTROL METHOS

In PV systems, there is only one MPP at each instant of time. Therefore, this system is constantly moving, and the MP is difficult to reach. Researchers propose using control methods to maintain the PV function at the MPP or around it to remedy this problem.

### A. P&O Method

The P&O technique hinges on the  $V_{PV}$  and the monitoring of the impact of this fluctuation on the PV harvest power [69]-[71]. The P&O method's workflow is shown in Fig. 5. To determine  $P_{PV}$  (k-1),  $V_{PV}$  and  $I_{PV}$  are calculated at each cycle (C). The value of  $P_{PV}$  (k-1) determined in the preceding C is contrasted with this  $P_{PV}$  (k). The  $V_{PV}$  is further regulated identically as the previous C if the level of power produced has risen. The  $V_{PV}$  is modified in the reverse manner as in the previous cycle if the electricity output has dropped. Consequently,  $V_{PV}$  is disrupted during every MPPT-C. The  $V_{PV}$  fluctuates about the ideal value  $V_{PV}$  until the MPP is obtained.

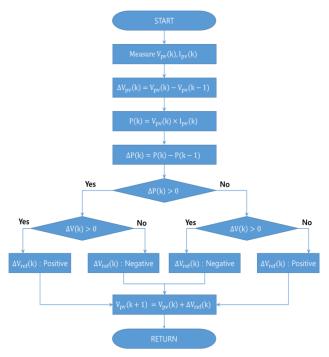


Fig. 5. The P&O workflow

#### B. INC Method

The P-V shape of the SC serves as the basis for the INC operation [72]-[74]. The MPP (point B) in Fig. 6, and the slope (S) is zero. We can observe from the MPP that the right side has a -S while the left side has a +S. Formulas (10)

through (12) display what's happening at every point. In Equations (10) - (12),  $I_{PV}$ ./ $V_{PV}$  is the conductance, and  $dI_{PV}/dV_{PV}$  is the IN of the alteration in conductance [51], [75]. INC flowchart shown in Fig. 7.

In general, the voltage from the source is positive to conclude the critical results of the INC method.

In point "A," The MP is on the left, so we must increment.

In point "B," We are on the MP.

In point "C," The MP is on the right, so we have to decrement.

$$\frac{\mathrm{dP}}{\mathrm{d}V_{pv}} = \frac{\mathrm{d}(V_{pv}I_{pv})}{\mathrm{d}V_{pv}} = I_{pv} + V_{pv}\frac{\mathrm{d}I_{pv}}{\mathrm{d}V_{pv}}$$
(9)

$$A: \frac{dP}{dV_{pv}} = I_{pv} + V_{pv} \frac{dI_{pv}}{dV_{pv}} < 0 \rightarrow \frac{dI_{pv}}{dV_{pv}} < -\frac{I_{pv}}{V_{pv}}$$
(10)

$$B: \frac{dP}{dV_{pv}} = I_{pv} + V_{pv} \frac{dI_{pv}}{dV_{pv}} = 0 \to \frac{dI_{pv}}{dV_{pv}} = -\frac{I_{pv}}{V_{pv}}$$
(11)

$$C \colon \frac{\mathrm{dP}}{dV_{pv}} = I_{pv} + V_{pv} \frac{dI_{pv}}{dV_{pv}} > 0 \to \frac{dI_{pv}}{dV_{pv}} > -\frac{I_{pv}}{V_{pv}} \tag{12} \label{eq:12}$$

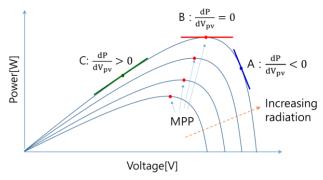


Fig. 6. P-V characteristic of PV cells

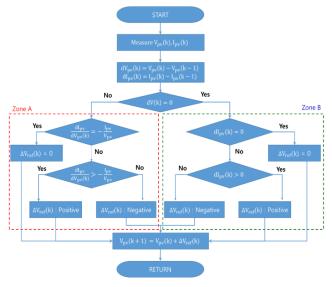


Fig. 7. INC flowchart

## C. FLC Method

The proposed FLC entails two inputs, which are: error (E), and dynamic error ( $\Delta E$ ). The input E(k) displays whether the scheme's working point is to the left or right of the MPP,

while the input  $\Delta E(k)$  displays the mark of the variation as illustrated in Table III. The output of the FLC-MPPT is the duty C of the BC  $\Delta D$ , so the control law is embodied as tails [76]-[80].

$$E = \frac{P(k) - P(k-1)}{V(k) - V(k-1)}$$
 (13)

$$\Delta E = E(k) - E(k-1) \tag{14}$$

The investigated scheme is presented in Fig. 8, Membership function plots for E,  $\Delta$ E, and  $\Delta$ D shown in Fig. 9, Characteristic surface of the FLC shown in Fig. 10.

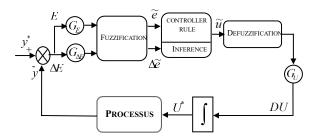


Fig. 8. Proposed control scheme

TABLE III. FLC RULE TABLE

<b>E</b> ( <b>k</b> )\ Δ <b>E</b> ( <b>k</b> )	ΔD				
E(R) ( \( \text{AE}(R) \)	NB	NS	ZE	PS	PB
NB	ZE	ZE	PB	PB	PB
NS	ZE	ZE	PS	PS	PS
ZE	PS	ZE	ZE	ZE	NS
PB	NS	NS	NS	ZE	ZE
PS	NB	NB	NB	ZE	ZE

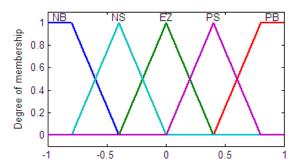


Fig. 9. Membership function plots for E,  $\Delta E$ , and  $\Delta D$ 

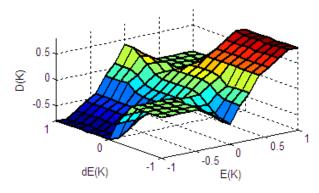


Fig. 10. Characteristic surface of the FLC

## IV. RESULTS AND DISCUSSIONS

Many simulations are run in MATLAB/Simulink to assess the suggested MPPT techniques' efficiency. The

response and precision data of the investigated methods are presented in Table IV. Furthermore, the performance evaluation of these methods is listed in Table V in terms of response time (RS), tracking accuracy (TA), and stability.

#### A. Case I

In conditions  $25\text{C}^\circ$  and  $1000 \text{ W} \backslash \text{m}^2$ , the results are represented in Fig. 11. From Fig. 11, we can see that the P&O reaches the MPP after a time of 0.33s and stays close to the MP. In the INC, we can see that the time to reach the MP is 0.79, but for the FLC, we can see that the FLC has a good time response equal to 0.11s. It is evident from this image, which compares the three methods, that the FLC produces results with high TA and acceptable RS.

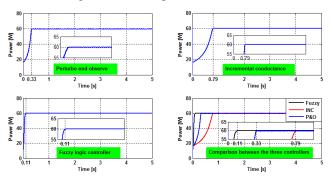


Fig. 11. Simulation results in atmospheric conditions 25C° and 1000 W\m<sup>2</sup>

#### B. Case II

For a constant temperature of  $25\text{C}^\circ$  and radiation varies from  $500 \text{ W/m}^2$  to  $1000 \text{ W/m}^2$ , the simulation results of the proposed controllers are given in Fig. 12. From Fig. 12, we can see that the P&O grasps the MPP after a time of 0.25s and stays around the MP. At the same time, in the case of irradiation, a change from  $500 \text{ W/m}^2$  to  $1000 \text{ W/m}^2$  takes a time of 0.06s to reach the MPP. Still, in the INC, we can see that the time to get the MP is 0.57s, and in irradiation, change takes a time of 0.17s and stays very close to the MPP. We can see that the FLC has a virtuous RS of 0.16s and 0.06s to reach the MPP in irradiation change from  $500 \text{ W/m}^2$  to  $1000 \text{ W/m}^2$ . The figure shows the comparison between the three controllers proves the efficiency of the FLC and that the increase of the irradiation generates an increase in the power.

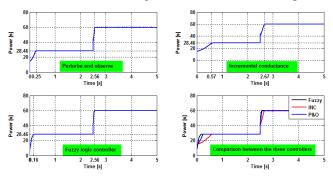


Fig. 12. Simulation results in atmospheric conditions 25C° and radiation varies from 500 W\m^2 to 1000 W\m^2

### C. Case III

For constant irradiation 1000 W\m² and temperature varies from 25C° to 50C°, Fig. 13 displays the computer simulation outcomes for the suggested MPPT methods. In the

temperature variation test we notice a good time of reaching the MPP but with an overshoot in all the controls, but still, the FLC-MPPT control is a good choice. The comparison made proves the efficiency of the FLC-MPPT.

TABLE IV. TIME RESPONSE AND PRECISION

Algorithms			
The conditions	P&O	INC	FLC
25C° and 1000 W/m <sup>2</sup>	0.33s	0.79s	0.11s
25C° and 500 W/m <sup>2</sup> to 1000	0.25s and	0.57s and	0.16s and
$W/m^2$	0.09s	0.17s	0.06s
25C°to 50C° and 1000 W/m <sup>2</sup>	Good time	Good time	Good time
Precision	Middle	Good	Very good

TABLE V. PERFORMANCE COMPARISON OF STUDIED METHODS

Methods	RS	TA	Stability
P&O	Medium (M)	Н	M
INC	High (H)	Н	M
FLC (proposed)	Very H (VH)	VH	VH

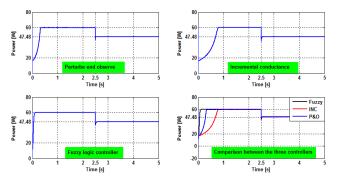


Fig. 13. Simulation results in atmospheric conditions temperature vary from  $25C^\circ$  to  $50C^\circ$  and  $1000~W\backslash m^2$ 

## V. CONCLUSION

Three approaches (P&O, INC, and FLC) to carrying out MPPT in PV systems were examined in this research. The FLC-MPPT method's performance was assessed and contrasted with that of other algorithms, including INC and P&O. The FLC-MPPT performed better than the formerly discussed methods and continuously showed outstanding tracking abilities in every situation. Additionally, it demonstrated a significant drop in power fluctuations, the lowest average tracking time of 0.06%, and a reduction of more than 60% in convergence time. Future research will focus on improving metaheuristic techniques to distinguish between patterns that are evenly and partly shaded.

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