

Robust Canonical Correlation Analysis on Leakage Current Behaviors of Geothermal Polluted Porcelain Insulators

(Analisis Korelasi Kanonik Robust dalam Kelakuan Arus Bocor Isolator Porselen Terpolusi Panas Bumi)

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ABSTRACT

This study presents the leakage current measurements results of three natural geothermal polluted porcelain insulators. The insulators consisted of one new-clean insulator, as reference, and three polluted insulators. The carried out measurements were leakage current and applied high voltage waveforms, used a two-channel storage digital oscilloscope, in a hermetically sealed chamber, where temperature, humidity, pressure and applied voltage amplitude could be adjusted and measured simultaneously. The leakage current waveforms were analyzed using the FFT and the statistical concerns were analyzed by the Fast-Minimum Covariance Determinant (FMCD) of robust multivariate statistical tools, and canonical correlation analysis (CCA). The result indicated that after the fundament, the second highest of harmonics leakage current were fifth harmonics. The leakage current waveforms were significantly influenced by humidity, besides pollution. The dependent or output variables are linear functions of independent or input variables. Based on CCA, the dependent parameters depended on input parameters tightly, with the canonical correlations were more than 0.99. The leakage current amplitudes were still predominantly influenced by applied voltage amplitudes, where the phase angles and THD were slightly influenced by relative humidity. On these experimental measurements, the insulators were still in normal operation.

Keywords: CCA, FMCD, geothermal, leakage current, porcelain insulator

INTRODUCTION

Overhead transmission or distribution lines are widely used in present power system to transmit electric power from generation stations to customer points. Their proper function depends on a large extent of insulation system with the supporting structures (Fernando, 1999). One can summarize the whole process as an interaction between the insulator, pollutants, wet conditions, and applied voltage. Thus, for a better understanding of insulator pollution, wetting and the flashover process, some terms should be studied. Some terms related to this case are the local climate and environmental (pollution) conditions surrounding the insulator with emphasis on wetting, pollution sources and type of pollution, and leakage currents (LCs) flowing over the surface of insulator (Vosloo, 2002).

One parameter of insulator performance is specified by leakage current. LCs were characterized by some parameters, such as amplitude, phase angle or power factor, each harmonics and THD, as outputs. These parameters were influenced by some inputs, such pollutant adhered on insulator surface, relative humidity, temperature, pressure and applied high voltage amplitude (Waluyo et al., 2008). Due to from naturally site, in this case the pollutant parameter is not included on the statistical computation. Nevertheless, it has been conducted some EDAX tests on naturally pollutant, from Kamojang area of geothermal power plant. As instead, it was discussed in narrative related to leakage current.

Transmission and/or distribution lines are also passed through geothermal areas. Geothermal power stations create emission as chemical materials, such as CO₂ and H₂S. Generally, CO₂ is the major component (94–98%), H₂S is around 1% and mercury concentration is as

high as 1–10 mg/Nm³. Typical concentrations of mercury and hydrogen sulfide were of the order of 10–20 ng/m³ and 20–40 µg/m³, respectively (Bacci et al., 2000).

Geothermal fluids (steam or hot water) usually contain some gasses, such as CO₂, H₂S, NH₃, CH₄, and trace amounts of other gasses, as well as dissolved chemicals whose concentrations usually increase with temperature. The dissolved chemical elements, such as sodium chloride (NaCl), boron (B), arsenic (As) and mercury (Hg) were source of pollution if discharged into the environment (Dickson et al., 2004).

The typical non-condensable gasses (NCG) content in the steam flashed off the geothermal fluid from Icelandic high-enthalpy reservoirs were SiO₂, Na, K, Mg, Ca, Cl, SO₄ and Fe (Eliasson et al., 2001). H₂S can reach moderate concentrations. The incineration process burns the gas from steam to convert H₂S to SO₂, the gases are absorbed in water to form SO₃ and SO₄ in solution. H₂S, HCl and CO₂ were undertaken (Hammons et al., 2004). This meant it was made consider due to the chemical element existence may be reaction to the surrounding environment.

As and Hg were existed in geothermal waters. Hg was occurred in geothermal systems due to the absorption of vapour and volcanic gasses into thermal waters. As and Hg dissolved in thermal fluids and concentrated in surface alterations. Chemical compositions of thermal waters were Cl, SO₄ and HCO₃ (Herdianita et al., 2008). A gas stream containing H₂S could be converted into commercially quality sulfuric acid (Matthiasdottir, 2006). The incineration process burns the gas, as part of steam, to convert H₂S to SO₂, absorbed in water to form SO₃²⁻ and SO₄²⁻ (Reed et al., 1995). Major element compositions hot pools, geysers and cold meteoric waters at El Tatio were Ca²⁺, Na⁺, Mg²⁺, K⁺, Cl⁻, SO₄²⁻, SiO₂, and tAlk. The tAlk, total alkalinity, is the excess of alkaline components. The minor and trace element composition ones were Al, As, B, Ba, Br, Co, Cr, Cs, Cu, Fe, I, Li, Mn, Mo, Ni, Rb, Sr, Tl and Zn (Corlecci et al., 2005).

Typical geothermal fluids with local shallow ground waters, are characterized by a relatively high concentration of K, Ca, NO₃, SO₄, and Cl (Marques et al., 2003). The waters were mostly acid with pH from 1.5 to 7.9 caused by elevated SO₄ from 10 to 5066 ppm and were

also elevated in most metals including Fe (0.05-753 ppm) and Al (0.03-390 ppm) but low in Cl (1.4-17.9 ppm) (Markusson et al., 2009). The H₂S from the steam is oxidized by the dissolved oxygen to form elemental sulfur or sulfuric acid (H₂SO₄) which lowers the pH value (Gunnarsson et al., 2006). The gas was exhausted from the O, taken geothermal power station was supplied to a specific hot solution in which a thermophilic sulfur oxidizing bacterium was cultured. In this solution, the bacterium converts the H₂S in the gases into H₂SO₄ (Hirowatari et al., 1995).

As additional information, mercury levels in lichens were within the background range (0.1-0.2 microg/g dw). On the contrary, at Airole, Hg concentrations (0.63-0.67 microg/g dw) were much higher than background. After the new geothermal power plant went into operation at Bagnore, lichen concentrations of Hg showed a 50% increase from 0.22 to 0.32 microg/g dw (Loppi, 2001). Boron removal after single stage regeneration with 10% H₂SO₄ was found to be possible (Gokcen et al., 2004). The typical of non-condensable gasses (NCG) consist mainly of CO₂ and NH₃ (97-99%) (Demirbas, 2002). H₂S content in NCG was 100-200 ppm (Kaygusuz and Kaygusuz, 2002). Geothermal power plants (GTPP) could release from the non-condensable fraction of the steams: CO₂ (98%), H₂S (1.5%), methane (0.4%), hydrogen (0.1%). The oxidation of H₂S to SO₂ and its subsequent reaction to sulphate ions within the atmospheric produces aerosols representing a major component of acid rain. GTPP could also release, from the non-condensable fraction of the steams, trace amounts (0.001%) of ammonia, radon, boron, arsenic, cadmium and antimony. Ammonia and mercury may also enter local waters from geothermal steam condensate (EcoLogo, 2008).

Above cited references indicated that geothermal power plant could produce some chemical elements of emission, which might influence to the surrounding environment. It was supposed those compounds or elements in a certain level might reduce outdoor insulator performance. However, until now, it is still rare to conduct a research concerning to geothermal emission phenomena. Based on this condition, it was important to carry out a research regarding insulator leakage current on a geothermal area. In this analysis data, it is necessary two statistical tools, Fast Minimum

Covariance Determinant (FMCD) and canonical correlation analysis (CCA). FMCD algorithm, based on the so-called C-step, is the most efficient from the computational viewpoint (Herwindiati et al., 2007). For running the experimental result data, it was used FMCD tool box to obtained the clean data. FMCD tool box has been built by Verboven and Hubert (Verboven & Hubert, 2009).

It was necessary to find clean data of experimental results statistically. The clean data were defined as data did have suspected outlier(s). It is difficult to detect outliers in p-variate data when $p > 2$ because one can no longer rely on visual inspection. Although it is still quite easy to detect a single outlier by means of the Mahalanobis distances, this approach no longer suffices for multiple outliers because of the masking effect, by which multiple outliers do not necessarily have large Mahalanobis distances. It is better to use distances based on robust estimators of multivariate location and scatter. In regression analysis, robust distances computed from the explanatory variables allow us to detect leverage points. Moreover, robust estimation of multivariate location and scatter are key tools to be robust, other multivariate techniques such as principal component analysis and discriminant analysis (Rousseeuw & Driessen, 1999).

In some sets of multivariate data, naturally variables are divided into two groups. CCA can be used to investigate relations between two groups, to identify and quantify groups between two sets of variables. CCA was early developed by H. Hotelling, in 1935-1936. CCA focuses on correlation between a linear combination of variables on one set, and a linear combination on other set. The ideas are determining linear combination pairs that have highest correlation. Furthermore, it is necessary for determining linear combination pairs that have highest correlation, after previous first choice, and so on. The linear combination pairs are called Canonical Variables, and their correlations are called Canonical Correlations. Canonical Correlations measure strength of relation between two variable sets. Technical maximized aspect represents an effort to concentrate a high dimensional relation between two sets into some canonical variables pairs. CCA is also study of relation between a

predictor (independent variables) variable set and response size set (dependent, criterion variables). In multiple regression approach to obtain a linear combination of original predictor variable, it describes variations of criterion size. CCA is used to analyze some predictor variables and criterion variables simultaneously (Johnson & Wichern, 2002; Manly, 1989; Dillon & Goldstein, 1984; Seber, 1984; Harris, 2001).

The objectives of research are to obtain the tendency of leakage current properties on porcelain insulators from the new-clean to nearly two years polluted conditions those installed on a geothermal power plant area. These properties are LC amplitudes, waveforms and phase angles. The relations among properties to environmental parameters are analyzed using robust canonical correlation analysis (CCA). It is called 'robust' because it was given precedence a data cleaning with Fast Minimum Covariance Determinant (FMCD) of robust multivariate statistical tools. As comparison, it is given some graphics which indicated some parameters of leakage current to some environmental parameters individually, especially to relative humidity.

EXPERIMENTAL AND ANALYSIS METHODS

These experiments were conducted on one new-clean and three polluted identical 20 kV outdoor porcelain insulators. The polluted insulators were some new-clean insulators which installed at PLN switchyard of Kamojang geothermal power plant, West Java, where is located around 1350 m above sea level, on December 14th, 2006 together, and then taken gradually, one by one, around 3 to 4 months later. The date of insulator withdrawal is mentioned on the chapter of experimental results, for each insulator.

The insulators were tested in a hermetically sealed chamber, where temperature, humidity, pressure and applied voltage could be adjusted and measured simultaneously. The size of the chamber was 120 cm x 150 cm x 120 cm (WxHxD). The measurements of leakage current and applied high voltage waveforms used a two-channel storage digital oscilloscope. The measured data could be recorded and transferred to a computer using USB and could be saved in softcopy form, i.e. in Excel and Bitmap forms. However, in this

manuscript, it is revealed in Excel graphical form only. The schematic diagram of experimental set up is shown in Figure 1. Furthermore, the data of LC waveforms were analyzed with fast Fourier transform (FFT), to obtain harmonic frequency spectra. The total harmonic distortion (THD) was defined as the total ratio of harmonic component amplitudes and the amplitude of fundamental frequency (Suwarno, 2006), as

$$THD = \frac{\sqrt{\sum_{n=2}^{\infty} I_n^2}}{I_1} \quad (1)$$

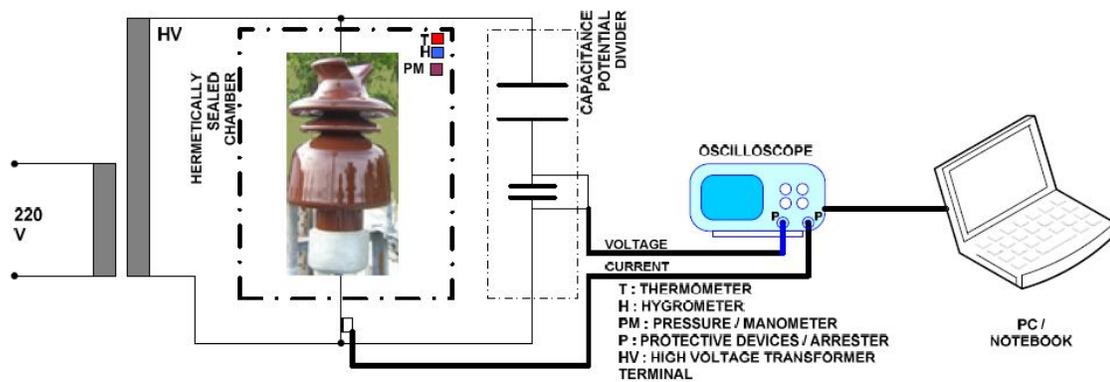


FIGURE 1. Schematic diagram of experimental set up

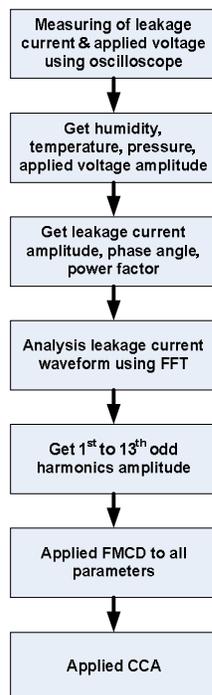


FIGURE 2. Flowchart of research and analysis methods

Thus, the frequency spectra were obtained on some conditions of insulators. These implementations used the Danielson-Lanczos method (Originlab Co., 2003). Furthermore, the data were analyzed by using FMCD to find the clean data and made correlations by using canonical correlation analysis (CCA). Figure 2 shows the flowchart of research and analysis methods. Firstly, the leakage current of new-clean and gradually polluted insulators were measured by using the oscilloscope.

Besides that, it was also read and noted the humidity, temperature and pressure. After the measurement steps, it was obtained leakage current amplitudes, phase angles and power factors or cosine of phase angle. Otherwise, the leakage current waveforms were analyzed by using FFT, to obtain 1st to 13th odd harmonics amplitudes. Finally, all above parameters were analyzed by using FMCD, and then CCA.

FMCD function is as filtering of clean data against to suspected outlier data. Whereas, CCA correlated between input (independent) data and output (dependent) data. In this case, the input parameters were applied voltage amplitude, humidity, temperature and pressure, and the output parameters were leakage current amplitude, phase angle, power factor, 1st to 13th odd harmonics amplitudes and THD. The block diagram between input and output parameters using CCA is shown in Figure 3.

Briefly, FMCD algorithm based on C-step is the most efficient from the computational viewpoint. Consider a data set $\{\bar{X}_1, \bar{X}_2, \dots, \bar{X}_n\}$ of

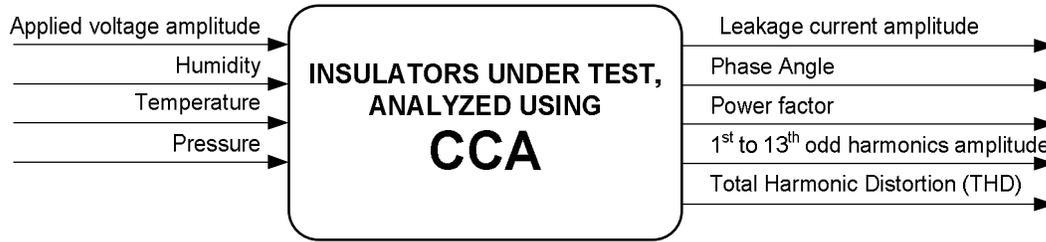


FIGURE 3. Input-output parameter black box diagram

p-variate observations. The FMCD algorithm is as follows (Herwindiati et al., 2007):

1. Let Hold be an arbitrary subset containing h data points.
2. Compute the mean vector $\bar{X}_{H_{old}}$ and covariance matrix $S_{H_{old}}$ of all observations belonging to H_{old} . Then, compute $d_{H_{old}}^2(i) = (\bar{x}_i - \bar{X}_{H_{old}})' S_{H_{old}}^{-1} (\bar{x}_i - \bar{X}_{H_{old}})$ for all $i = 1, 2, \dots, n$.
3. Sort these squared distances in increasing order, $d_{H_{old}}^2(\pi(1)) \leq d_{H_{old}}^2(\pi(2)) \leq \dots \leq d_{H_{old}}^2(\pi(n))$ where π is a permutation on $\{1, 2, \dots, n\}$.
4. Define $H_{new} = \{\bar{x}_{\pi(1)}, \bar{x}_{\pi(2)}, \dots, \bar{x}_{\pi(h)}\}$.
5. Calculate $\bar{X}_{H_{new}}, S_{H_{new}}, d_{H_{new}}^2(i)$.
6. If $\det(S_{H_{new}}) = 0$, repeat steps 1-5. If $\det(S_{H_{new}}) = \det(S_{H_{old}})$, the process is stopped. Otherwise, the process is continued until the kth iteration if $\det(S_{H_k}) = \det(S_{H_{k+1}})$. Thus, $\det(S_{H_1}) \geq \det(S_{H_2}) \geq \dots \geq \det(S_{H_k}) = \det(S_{H_{k+1}})$.

EXPERIMENTAL RESULTS, ANALYSIS AND DISCUSSION

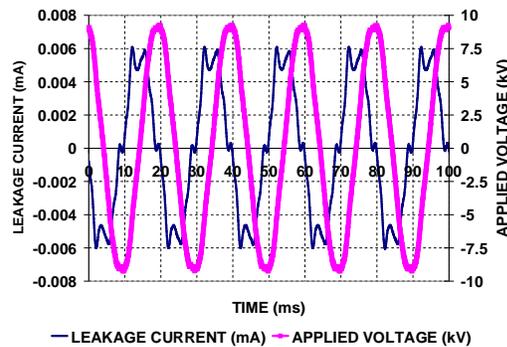
The Results from New-Clean Porcelain Insulator

There were many data on these measurement results. Nevertheless, it is presented two significant conditions only, namely dry (low humidity) and wet (high humidity). Due to similar behaviour for the leakage current waveforms on dry or low humidity conditions, it is only shown one leakage current waveform on those conditions. However, it is shown the leakage current waveforms on high humidity for each withdrawal of polluted insulators.

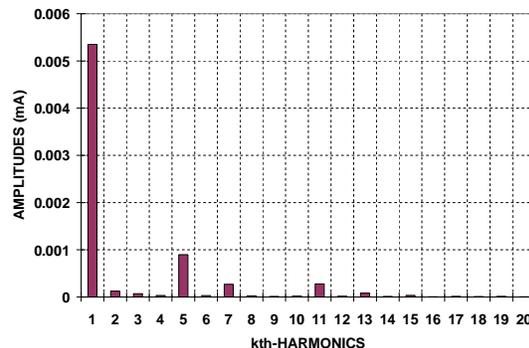
Figure 4(a) shows the leakage current and applied voltage waveforms of new-clean

insulator on the conditions of 67%, 26.7 centigrade, -0.8 kPa and 9.24 kV for relative humidity, temperature, pressure and maximum applied voltage respectively. The 67% of relative humidity was as dry typical condition.

From the leakage current and applied voltage waveforms, it was obtained a difference of angle, usually called phase angle, was 81.3 degree. It meant that the insulator in new, clean and dry condition was very capacitive.



(a) Leakage current wave

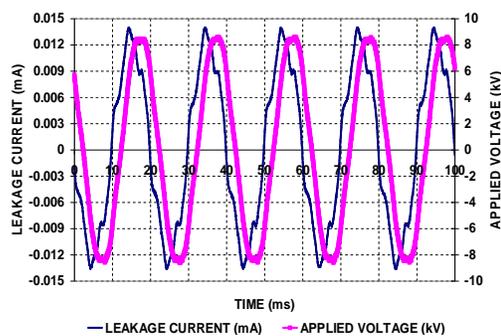


(b) Frequency spectrum of leakage current

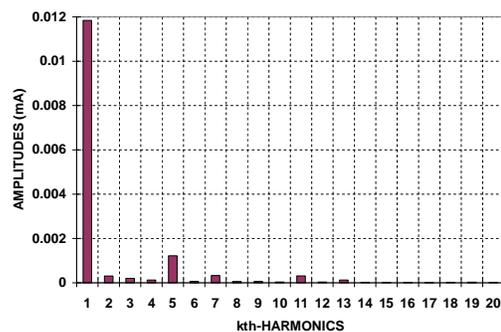
FIGURE 4. The LC wave and frequency spectrum of LC of dry new-clean insulator

Whereas, Figure 4(b) shows the corresponding leakage current frequency spectrum harmonics. In this condition, the first to thirteenth odd harmonics were 87.87%, 1.28%, 14.93%, 4.26%, 0.19%, 4.87% and 1.13% respectively compared to the leakage current wave amplitude. Moreover, based on these harmonics, it was calculated THD which resulted 18.6%.

Furthermore, Figure 5(a) shows the leakage current and applied voltage waveforms of new clean insulator in 99% of relative humidity, 26.7 centigrade of temperature, no pressure and 8.6 kV maximum applied voltage conditions. The 99% of relative humidity, or called high humidity, was as typical of wet condition.



(a) Leakage current wave



(b) Frequency spectrum of leakage current

FIGURE 5. The leakage current wave and its frequency spectrum of high humidity new-clean insulator

From this figure, it is shown that the leakage current waveform was different from the previous low humidity typical condition. The peaks of wave became sharper, and the phase angle, i.e. the angle was between leakage current and applied voltage waves, became smaller. This indication tends to approach a pure sinusoidal waveform relatively rather than that low humidity one. From both leakage

current and applied voltage waves, it was obtained the phase angle of 46.7 degree. This number was obtained from the calculation of leakage current and applied voltage experimental measurement. The amplitude of leakage current wave became higher than the previous low humidity condition. This phenomenon was dominantly caused by high humidity conditions. Thus, the high relative humidity made the new-clean porcelain insulator became little more conductive, rather than that dry condition. Nevertheless, the leakage current wave was not until pure sinusoidal waveform, and the wave did not coincide to the applied voltage wave. It meant the insulator did not reach a pure resistive property. The capacitive property was still dominant.

Moreover, Figure 5(b) shows the frequency spectrum of leakage current on the high humidity new-clean porcelain insulator. The first to thirteenth odd harmonic amplitudes were 85.8%, 1.43%, 8.84%, 2.39%, 0.43%, 2.26% and 0.89% respectively compared to the amplitude leakage current wave. Especially the percentage of fifth harmonic amplitude had reduced, from 14.93% became 8.84%. THD became 11.2%, from previous 18.6%. This meant the leakage current wave tent to close a pure sinusoidal wave compared to the previous condition. Nevertheless, the insulator still worked normally, although the third harmonic had increased. Usually, a non normality of insulator performance is indicated by third harmonic amplitude which is very high, beside the leakage current amplitude which very high.

Figure 6 shows test result scatter plots of FMCD or robust distance. Based on the robust test, the suspected outlier data were sequential data of 1-8, 10, 13-16 and 7 last data. Generally, it is seen the result data of FMCD robust distance were mostly grouping distinctly under cut-off line. The under cut-off line data were not suspected as outlier data, which were taken account on CCA.

Figure 7 shows the canonical result scatter plot based on robust distance for new-clean porcelain insulator. In this case, the first canonical correlation was 0.99466. This value, closed to unity, indicated that the correlation between independent and dependent variables was very very high. Statistically, this case revealed that the output variables almost depended on input variables, as 99.466%.

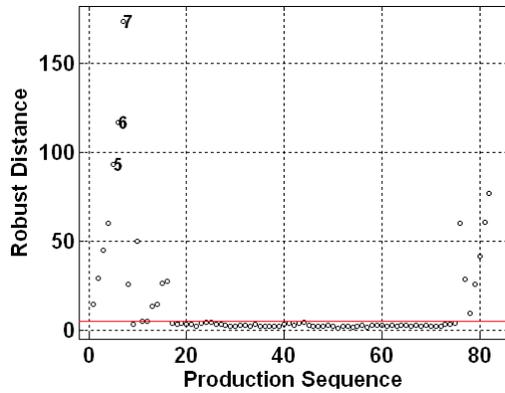


FIGURE 6. Robust distance results on LC data of new-clean insulator

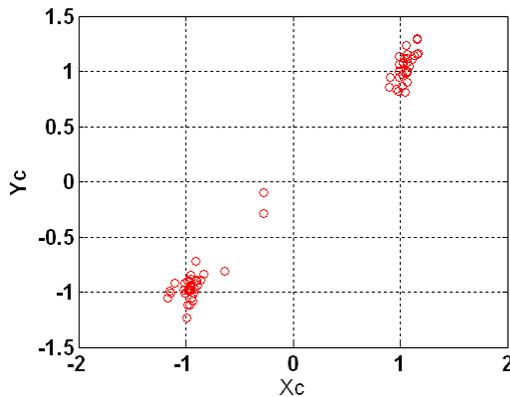


FIGURE 7. Canonical result scatter plot based on FMCD of new-clean insulator

Based on canonical variates for corresponding canonical correlation, the horizontal axis X_c was $0.008636 \cdot H + 0.0231467 \cdot T + 0.014693 \cdot P - 1.0038348 \cdot V_{max}$, where H , T , P and V_{max} are relative humidity, temperature, pressure and applied voltage amplitude respectively. It is indicated that the influence of applied voltage was very significant to dependent parameters. Whereas, Y_c was $848.7 \cdot I_{max} + 1.14 \cdot PHI + 70.7 \cdot PF - 759.2 \cdot H_1 + 2677.7 \cdot H_3 - 2819.9 \cdot H_5 + 1014.6 \cdot H_7 - 1850.9 \cdot H_9 - 2523.4 \cdot H_{11} - 1032.6 \cdot H_{13} - 13.7 \cdot THD$, where I_{max} , PHI , PH , H_1 - H_{13} and THD were leakage current amplitude, phase angle, power factor, first to thirteenth odd harmonics and total harmonic distortion respectively. It is indicated that leakage current amplitude was influenced by input parameters, especially by applied voltage amplitude, very considerably.

It is indicated that the scatter plots tent to concentrate on a straight line and balance between positive and negative of axes. These phenomena indicated that the output parameters highly depended on the input

parameters. If it is made regressions with one and five powers, the regression equations were

$$Y_c = 0.99466 X_c, \text{ and}$$

$$Y_c = 0.3182 X_c^5 + 0.389 X_c^4 - 0.7956 X_c^3 - 0.6138 X_c^2 + 1.457 X_c + 0.22$$

respectively. The line regression lines tent to be linear.

Both equations are different explicitly. However, if it was made curves, it would show linear lines. Based on data analysis, the high coefficients of output parameters were leakage current amplitude and third harmonics amplitude of leakage current. These two parameters were especially contributed by applied voltage amplitude and humidity.

As a descriptive comparison, it is also presented the leakage current amplitude and phase angle, as shown on Figure 8, and total harmonic distortion (THD), as shown on Figure 9, as function of relative humidity on the experimental results of new-clean porcelain insulator. The leakage current amplitude would increase slightly as relative humidity rose. Otherwise, the phase angle would reduce if relative humidity increased. The latter of reducing phase angle was significantly enough. Whereas, the THD would decrease if relative humidity increased.

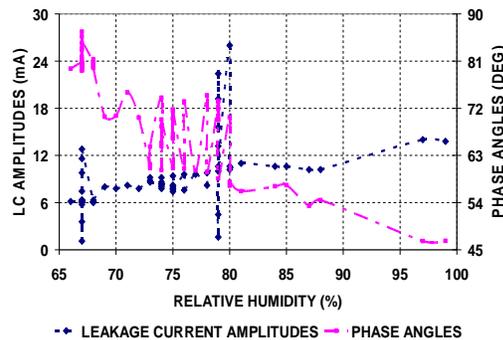


FIGURE 8. Leakage current amplitude and phase angle vs relative humidity of new-clean insulator

The results from first withdrawal polluted porcelain insulator

The polluted insulators were first to third withdrawal of porcelain insulators after polluted on site of geothermal power plant. In general, on dry typical conditions, the leakage current waveforms and other behaviors were similar with the previous new clean insulator, so that, it will not be shown anymore.

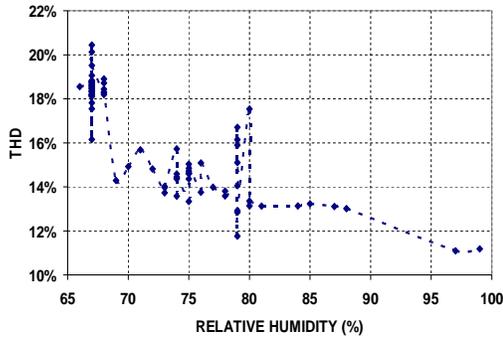
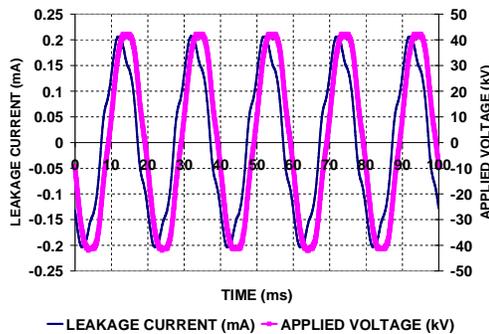


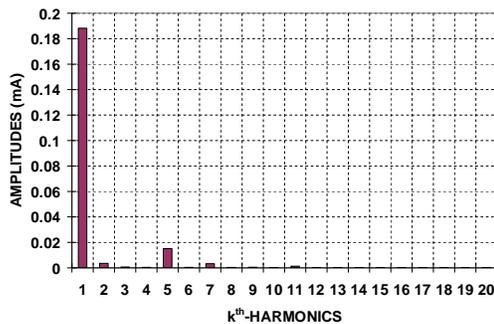
FIGURE 9. Total harmonic distortion (THD) vs relative humidity of new-clean insulator

Nevertheless, on high relative humidity, they were significantly different. Thus, it is presented the waveforms on high humidity only.

On the first removal porcelain insulator, it was carried out on 31th August 2007, the waveforms are shown in Figure 10(a). This condition was 90%, 34.5°C and 42 kV_{max} for relative humidity, temperature and applied voltage amplitude respectively, and without pressure. The odd harmonics were 91.4%, 0.4%, 7.3%, 1.6%, 0.2%, 0.1% and 0.1% to leakage current amplitude, 206 μA.



(a) Leakage current and applied waves



(b) Leakage current frequency spectrum

FIGURE 10. The LC wave and frequency spectrum of high humidity first withdrawal polluted insulator

Otherwise, the impedance, THD and phase angle were 203,883,495 Ω, 8.26% and 35.6 degree respectively. It is shown that the leakage current waveform was more pure sinusoidal than that on dry condition. The leakage current amplitude was higher than that on low humidity. It was the closest to pure sinusoidal waveform among other waveforms.

The approach to pure sinusoidal waveform property is also indicated by frequency spectrum in Figure 10(b). It is shown that after fundamental, the second highest is fifth harmonics, which is very small, indicated that the leakage current waveform tend to be pure sinusoidal relatively.

Figure 11 shows test result scatter plots of robust distances of first withdrawal polluted insulator leakage current data. Based on the robust test, the suspected outlier data were sequential data of 1,2,8,15,20 and 36 sequential data.

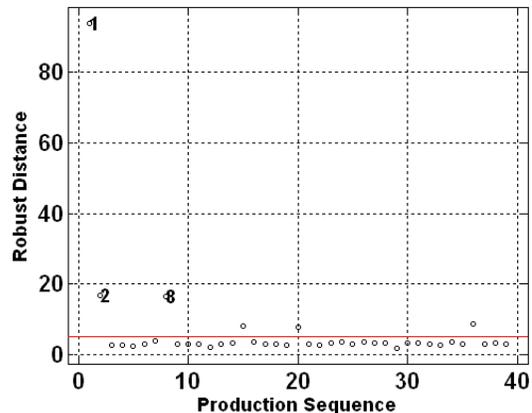


FIGURE 11. Robust distance results on leakage current data of first withdrawal polluted insulator

Figure 12 shows the canonical scatter plot based on robust distance of leakage current for first withdrawal geothermal polluted porcelain insulator. In this case, the canonical correlation is 0.9989. This value, closed to unity, indicated that the correlation between independent and dependent variables was very very high. Statistically, this case revealed that the output variables almost depended on input variables, as 99.89%.

The horizontal axis X1 was $-0.0001225 \cdot H - 0.0724227 \cdot T - 0.124997 \cdot P - 0.991497 \cdot V_{max}$. It is also indicated that the influence of applied voltage was very significant to dependent parameters. Whereas, the vertical axis Y1 was $14.14 \cdot I_{max} + 1.272 \cdot \text{PHI} + 105.75 \cdot \text{PF} + 44.4 \cdot H_1 + 480.3 \cdot H_3 - 501.1 \cdot H_5 - 429.1 \cdot H_7 +$

$1068.3 \cdot H_9 - 1645 \cdot H_{11} + 220 \cdot H_{13} + 0.66 \cdot THD$, where I_{max} , PHI, PH, H_1 - H_{13} and THD were leakage current amplitude, phase angle, power factor, first to thirteenth odd harmonics and total harmonic distortion respectively. It is indicated that leakage current amplitude was influenced by input parameters, especially by applied voltage amplitude, very considerably.

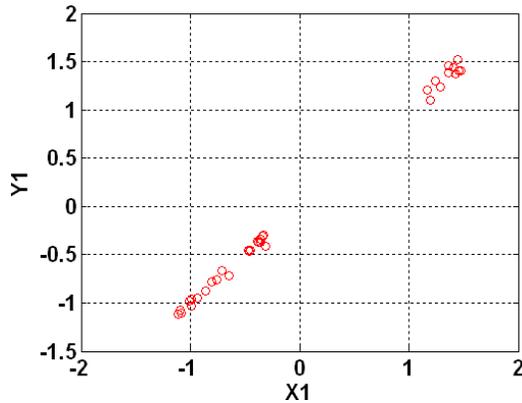


FIGURE 12. Canonical result scatter plot based on FMCD of first withdrawal polluted insulator

It is indicated that the scatter plots tend to concentrate on a straight line and balance between positive and negative of axes. These phenomena indicated that the output parameters highly depended on the input parameters. If it is made regressions with one and five powers, the regression equations were

$$Y_1 = 0.9989 X_1, \text{ and}$$

$$Y_1 = -0.205 X_1^5 + 0.0775 X_1^4 - 0.5425 X_1^3 - 0.012256 X_1^2 + 0.61886 X_1 - 0.1168,$$

respectively. The line regression lines tend to be linear.

Both equations are different explicitly. However, if it was made curves, it would show linear lines. Based on data analysis, the high coefficients of output parameters were leakage current amplitude, power factor and third harmonics amplitude of leakage current. These three parameters were especially contributed by applied voltage amplitude and humidity. The effect of humidity and applied voltage reduced rather than that the new-clean insulator. This case was caused by influence of pollutant on insulator surface. The dry season was in progress, when withdrawal of insulator.

As a descriptive comparison, it is also presented the leakage current amplitude and phase angle, as shown on Figure 13, and total harmonic distortion (THD), as shown on

Figure 14, as function of relative humidity on the experimental results of first withdrawal porcelain insulator. The leakage current amplitude would increase very slightly as relative humidity rose. Otherwise, the phase angle would reduce significantly enough if relative humidity increased. Whereas, the THD would decrease slightly if relative humidity increased.

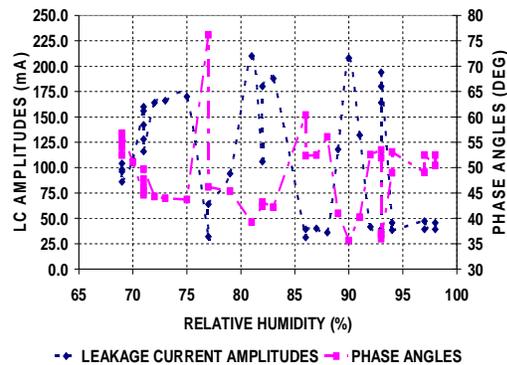


FIGURE 13. Leakage current amplitude and phase angle vs relative humidity of first withdrawal insulator

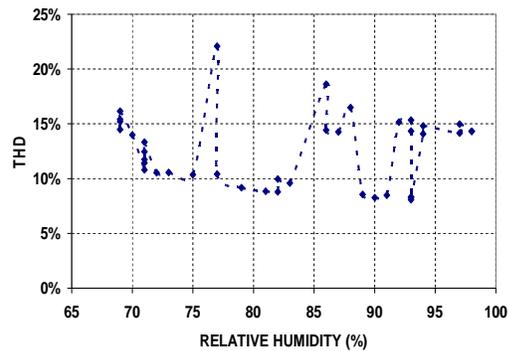


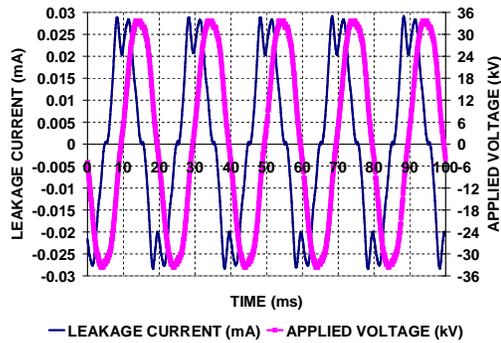
FIGURE 14. Total harmonic distortion (THD) vs relative humidity of first withdrawal insulator

The Results from Second Withdrawal Polluted Porcelain Insulator

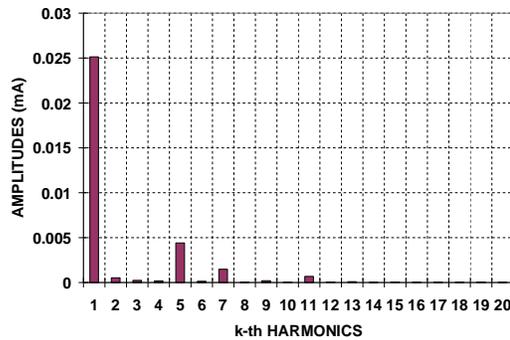
Whereas, Figure 15(a) shows the waveforms of second withdrawal porcelain insulator on high humidity condition (on 4th December 2007). These waveforms were measured on 99%, 28.9°C, 34.4 kV_{max} for relative humidity, temperature and applied voltage amplitude, and without pressure.

Figure 15(b) shows the leakage current harmonic frequency spectrum. The harmonics were 23.9 μA, 0.2 μA, 4.3 μA, 1.47 μA, 0.22 μA, 0.65 μA and 0.12 μA, and the leakage current amplitude was 27.6 μA. Then, THD

and phase angle were 19.3 % and 66.8 degree, respectively.



(a) Leakage current and applied voltage waves



(b) Leakage current frequency spectrum

FIGURE 15. The leakage current wave and frequency spectrum of high humidity second withdrawal polluted insulator

It is shown that fifth and seventh harmonics were also dominant, after the fundamental. These occurrences were caused by the leakage current waveform on Figure 15(a) which was rather far from pure sinusoidal waveform. In this condition, the insulator was still in capacitive property, due to less of pollutant on the insulator surface. This was caused by the withdrawal of insulator was conducted in rainy season. Thus, the insulator was still relatively clean, so that effect of high humidity was relatively low.

Based on the robustness test result, it was revealed the script like as below. Thus, there was not detected a suspected outlier.

```

Minimum Covariance Determinant Estimator.
The 94-th order statistic of the absolute deviation of variable 3
is zero.
There are 110 observations in the entire dataset of 121
observations that lie on the
hyperplane with equation a_1 (x_i1-m_1) + ... + a_p (x_ip-m_p) =
0
with coefficients a_i equal to :
0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0
and where the mean (m_1,...,m_p) of these observations is the MCD
location.
    
```

Figure 16 shows the canonical scatter plot based on robust distance of leakage current for second withdrawal geothermal polluted porcelain insulator. In this case, the canonical correlation was 0.9989.

The horizontal axis X₂ is $-0.0033737 * H - 0.0011185 * T - 0.031927 * P + 0.07782 * V_{max}$. Whereas, the vertical axis Y₂ is $0.0553 * I_{max} + 0.08317 * PHI + 5.0487 * PF - 0.084 * H_1 - 0.145 * H_3 + 0.48866 * H_5 + 0.0897 * H_7 + 0.125 * H_9 + 1.0221 * H_{11} + 1.1 * H_{13} - 0.0277 * THD$.

Based on these equations, the applied voltage amplitude was most dominant among other input parameters. Otherwise, the most dominant of output parameters was power factor or phase angle. The latter case meant the power factor or phase angle had most change due to various input parameters, among other output parameters. If it is made regressions with one and five powers, the regression equations were

$$Y_2 = 0.9958 X_2, \text{ and}$$

$$Y_2 = -0.003655 X_2^5 + 0.005 X_2^4 + 0.03386 X_2^3 - 0.013787 X_2^2 + 0.9433 X_2 + 0.00727,$$

where Y₂ and X₂ are ordinate and abscissa, respectively.

Although, both mathematical equations are different, actually both graphical lines are similar as linear.

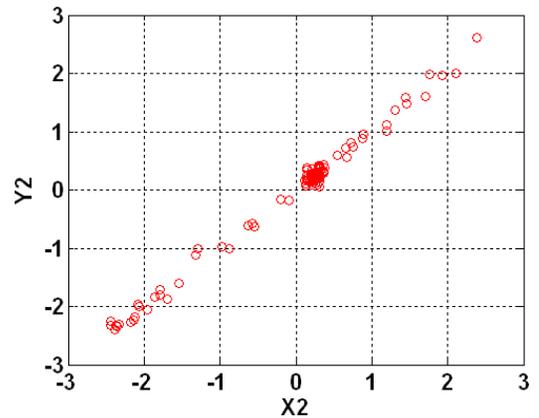


FIGURE 16. Canonical result scatter plot based on FMCD of second withdrawal polluted insulator

It is also presented the leakage current amplitude and phase angle, as shown on Figure 17, and total harmonic distortion (THD), as shown on Figure 18, as function of relative

humidity on the experimental results of second withdrawal porcelain insulator. The leakage current amplitude would increase very very slightly, or be practically linear, as relative humidity rose. Otherwise, the phase angle would reduce slightly if relative humidity increased. Whereas, the THD would decrease very slightly if relative humidity increased.

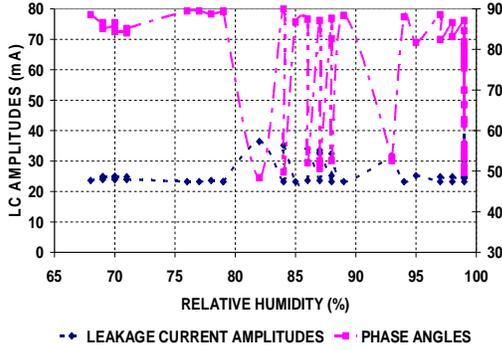


FIGURE 17. Leakage current amplitude and phase angle vs relative humidity of second withdrawal insulator

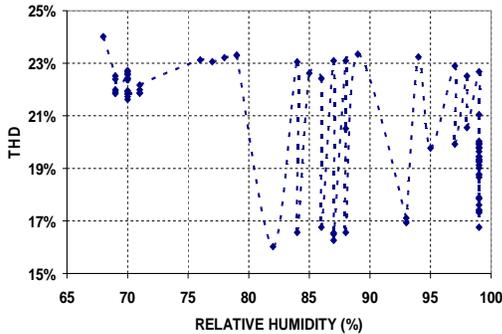


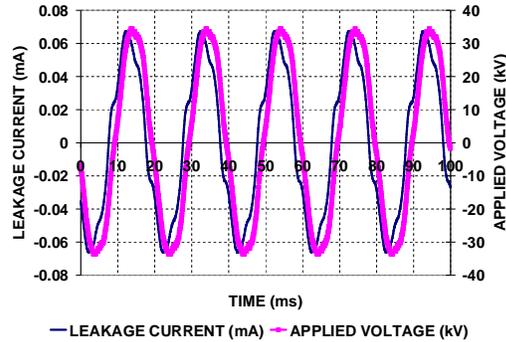
FIGURE 18. Total harmonic distortion (THD) vs relative humidity of second withdrawal insulator

The Results from Third Withdrawal Polluted Porcelain

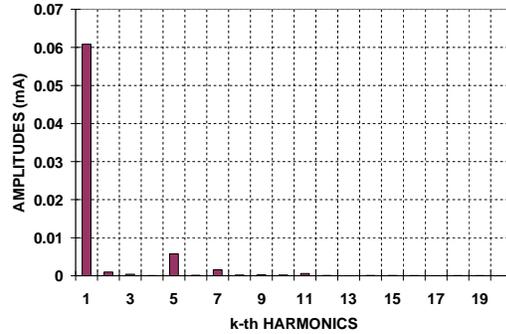
Figure 19(a) presents the leakage current and applied voltage waveforms of porcelain insulator for third withdrawal on 18th March 2008. The condition of measurement was 99%, 25.8°C, 15.6kPa, and 34.44 kV_{max} for relative humidity, temperature, pressure and applied voltage respectively. On this condition, the leakage current amplitude and phase angle were 67.2 μA and 25.69° respectively. It is seen that the phase angle was small, indicated by the leakage current wave is so close to applied voltage wave.

Figure 19(b) shows the leakage current frequency spectrum on that condition. The

harmonic amplitudes were 60.83 μA, 0.405 μA, 5.77 μA, 1.60 μA, 0.292 μA, 0.609 μA and 0.028 μA for first to thirteenth odd harmonics respectively. In percentage, these were 90.52%, 0.60%, 8.59%, 2.38%, 0.43%, 0.91% and 0.04%, while THD was found to be 9.93%. This value was so small, due to the leakage current waveform closed to sinusoidal form.



(a) LC and applied voltage waves



(b) LC frequency spectrum

FIGURE 19. The LC wave and frequency spectrum of wet third withdrawal polluted insulator

It is shown that fifth and seventh harmonics were also dominant, after the fundamental. However, their percentages to fundamental were lower than the second withdrawal. This meant the LC waveform was more pure sinusoidal rather than the second withdrawal, both on high humidity.

Figure 20 shows the test result scatter plots of robust distances of third withdrawal polluted porcelain insulator. Based on the robust test, the suspected outlier data were data number of 28-34, 36-40, 55 and 80-83.

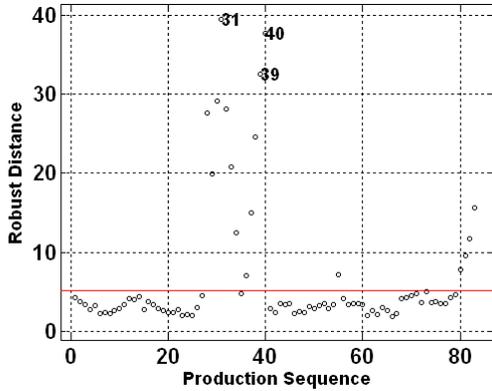


FIGURE 20. Robust distance results on leakage current data of third withdrawal polluted insulator

Figure 21 shows the canonical scatter plot based on robust distance of leakage current for third withdrawal geothermal polluted porcelain insulator. In this case, the canonical correlation was 0.9917.

The horizontal axis X3 is $0.0026 \cdot H + 0.134 \cdot T + 0.033 \cdot P + 0.1623 \cdot V_{max}$. Whereas, the vertical axis Y3 is $0.0091 \cdot I_{max} + 0.11996 \cdot PHI + 6.3 \cdot PF + 0.04 \cdot H_1 - 1.65 \cdot H_3 + 0.8045 \cdot H_5 + 0.1663 \cdot H_7 - 0.3514 \cdot H_9 - 0.23 \cdot H_{11} + 0.44 \cdot H_{13} + 9.65 \cdot THD$.

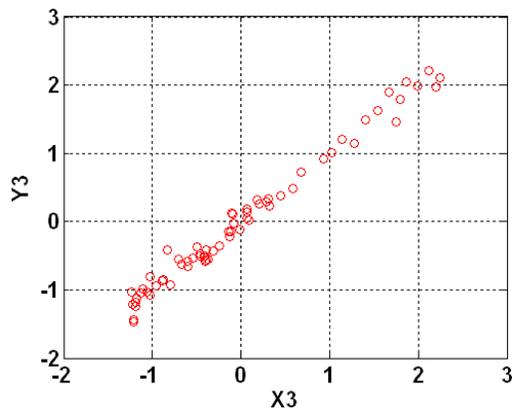


FIGURE 21. Canonical result scatter plot based on FMCD of third withdrawal polluted insulator

Based on the horizontal axis, the most dominant influence of input parameters was also applied voltage amplitude. Otherwise, the significant influence of output parameters were total harmonic distortion (THD) and power factor. Both latter output parameters were most change due to various change of output parameters. If it is made regressions with one and five powers, the regression equations were

$$Y_3 = 0.9917 X_3, \text{ and}$$

$$Y_3 = 0.0032 X_3^5 - 0.034 X_3^4 + 0.0221 X_3^3 + 0.0769 X_3^2 + 0.976 X_3 - 0.01896$$

respectively, where Y_3 and X_3 are ordinate and abscissa respectively.

Although, both mathematical equations are different, actually both graphical lines are fairly linear. Thus, the high power of polynomial equations did not influence significantly.

It is also presented the leakage current amplitude and phase angle, as shown on Figure 22, and total harmonic distortion (THD), as shown on Figure 23, as function of relative humidity on the experimental results of third withdrawal porcelain insulator. The leakage current amplitude would be practically linear, as relative humidity rose. Otherwise, the phase angle would reduce very slightly if relative humidity increased. Whereas, the THD would decrease very slightly if relative humidity increased.

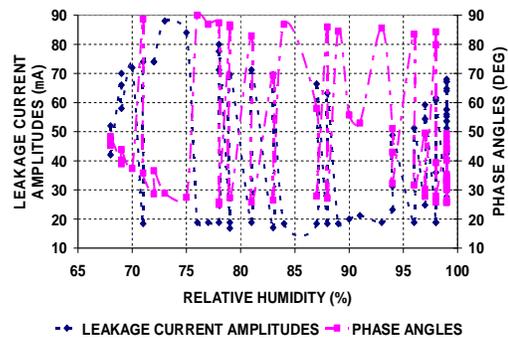


FIGURE 22. Leakage current amplitude and phase angle vs relative humidity of third withdrawal insulator

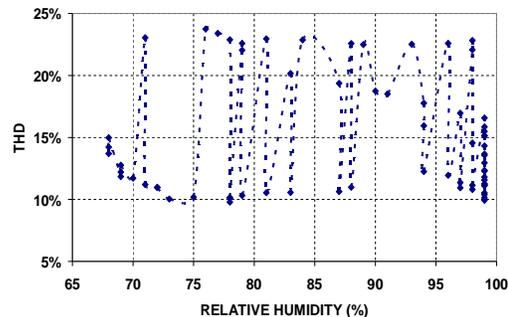


FIGURE 23. Total harmonic distortion (THD) vs relative humidity of third withdrawal insulator

Based on above data and analysis, it can be seen that the porcelain insulators were significantly influenced by humidity. The amplitudes of leakage current would increase

and phase angles would reduce as the humidity rise. These cases were explicitly indicated on high humidity, especially close to 99% of relative humidity. Nevertheless, the leakage current waves did not coincide to applied voltage wave. This was indicated that although the porcelain insulators were susceptible to humidity, and also to pollution, the geothermal switchyard area where taken as place of research, had medium pollution. Thus, the pollutant slightly influenced to leakage current of insulators.

Although, the porcelain insulators were influenced by humidity, in these cases, the leakage current amplitudes were still dominantly influenced by applied voltage amplitude. Nevertheless, the phase angles and total harmonic distortion (THD) of leakage current were significantly influenced by relative humidity. Generally, the phase angles and THD would reduce if the relative humidity increased. These cases meant that the insulators would be slightly more resistive rather than capacitive. However, on the high relative humidity, around 99%, the insulators were still dominated by capacitive property.

Refer to harmonics analysis, all second highest of harmonic amplitudes after fundamental frequency were fifth harmonics. Nevertheless, their percentages to fundamental frequency were different, depended on leakage current waveforms. Furthermore, the leakage current waveforms depended on environmental conditions, especially relative humidity. If the relative humidity was increased, the percentage of fifth harmonics to fundamental frequency of leakage current would reduce, due to the leakage current waveforms fairly tent to be close to pure sinusoidal.

Using fast minimum covariance determinant (FMCD), it is seen that some data were suspected as outliers. Usually, the suspected outliers were the different applied voltage considerably among other data, too high or too low. Thus, the suspected outlier data did not include to further analysis, namely canonical correlation analysis (CCA). On this using of CCA, the independent variables were applied voltage amplitude, relative humidity, temperature, and pressure. Otherwise, the dependent variables were leakage current amplitude, phase angle, power factor, 1st to 13th odd harmonics amplitudes and THD. The dependent or output variables are linear

functions of independent or input variables. These meant the output parameters depended upon the input parameters considerably. Based on CCA, the dependent parameters depended upon input parameters tightly, indicated by the all canonical correlations were more than 0.99, closed to unity. The leakage current amplitudes were still dominantly influenced by applied voltage amplitudes, where the phase angles and THD were slightly influenced by relative humidity. On these experimental measurements, the insulators were still in normal operation.

The independent variables, including their canonical variates, are placed on the abscissas and dependent variables are placed on the ordinates. All relations of dependent variables to independent variables are linear. Therefore, with certain canonical correlations and canonical variates, it can be said that independent variables influenced to change the dependent variables almost linearly. Physically, it was indicated that the changes of applied voltage amplitude, humidity, temperature and/or pressure would change the leakage current amplitude, phase angle, power factor, 1st to 13th odd harmonics and/or THD were fairly linearly too, and the output parameters were considerably depended on the independent parameters. Thus, the insulators, when the measurements were in progress, work in normal conditions.

CONCLUSIONS

Based on some experimental and analysis studies, it can be concluded some items;

- After the fundamental, the second highest of harmonics of leakage current were fifth harmonics. Their percentages were determined by leakage current waveforms.
- The leakage current waveforms were significantly influenced by humidity, besides pollution.
- In these porcelain insulators, the leakage current amplitudes were still dominantly influenced by applied voltage amplitudes.
- Based on FMCD, the suspected outlier data were usually the data which the applied voltage amplitudes were very far among data, too high or too low.
- On the CCA results, the dependent parameters were linear functions of independent parameters, on various

canonical variates. These meant the output parameters were very tightly influenced by input parameters, indicated also by the canonical correlations which more 0.99. As additional information from this case, It indicated that the insulators were still in normal operation.

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